

# 1 Observing and Modeling Earth's Energy Flows, 2 Thirteen Years Later

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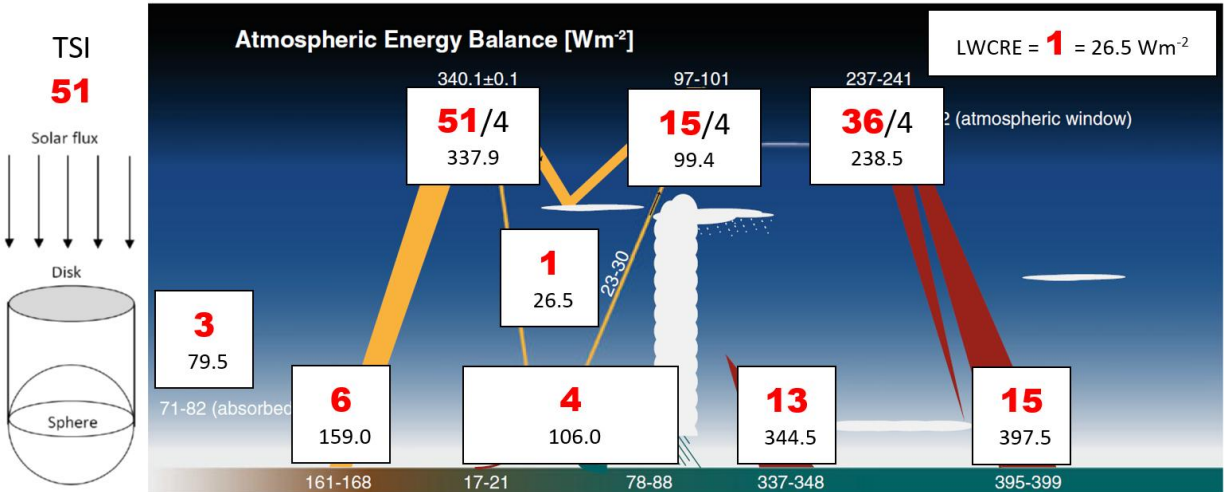
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6 **Abstract** Observing and modeling energy flows in Earth's climate system was reviewed in an  
7 article in *Surveys in Geophysics* thirteen years ago as a concluding paper of a special collection  
8 with the same title. Analyzing their global mean energy budget estimate, a remarkable recognition  
9 can be made: there are specific small integer ratios among the flux components, as each of them  
10 are very close to an integer multiple of a unit flux, which is the longwave cloud radiative effect  
11 (LWCRE) with a value of  $26.5 \text{ Wm}^{-2}$ , as given in that study. Similar global energy budget  
12 estimates later by other authors, the IPCC and the NASA CERES science team show the same  
13 structure with convincing accuracy: typically, within the stated ranges of uncertainty. The physical  
14 science basis for the core flux components is identified in four radiative transfer constraint  
15 equations having their origin in the long-known two-stream approximation of Schwarzschild's  
16 equation; the fundamental integer ratios are solutions of the set of these four equations.

17 **Keywords:** global mean energy flow systems; integer relationships; radiative transfer equations

## 18 Introduction

19 A review article was published in *Surveys in Geophysics* thirteen years ago as a concluding study  
20 of a special collection with the same title (Stevens and Schwartz, 2012). Projecting longwave cloud  
21 radiative effect (LWCRE) on the energy flow distribution with the given CERES value of  $26.5$   
22  $\text{Wm}^{-2}$ , it is easy to recognize that the flux components are integer multiples of that unit flux, close  
23 to the stated ranges of uncertainty; see Fig. 1.



1

2 **Fig. 1** Earth's global and annual mean energy flow system. Values are presented as a two-sigma range ( $\text{Wm}^{-2}$ ).  
 3 Original: Stevens and Schwartz (2012). We inserted LW CRE from their study, with their value from CERES  
 4 EBAF. Numbers in red bold typeface are expressed in the unit of  $26.5 \text{ Wm}^{-2}$ . TOA fluxes are integers on the  
 5 intercepting cross-section disk of incoming solar radiation.

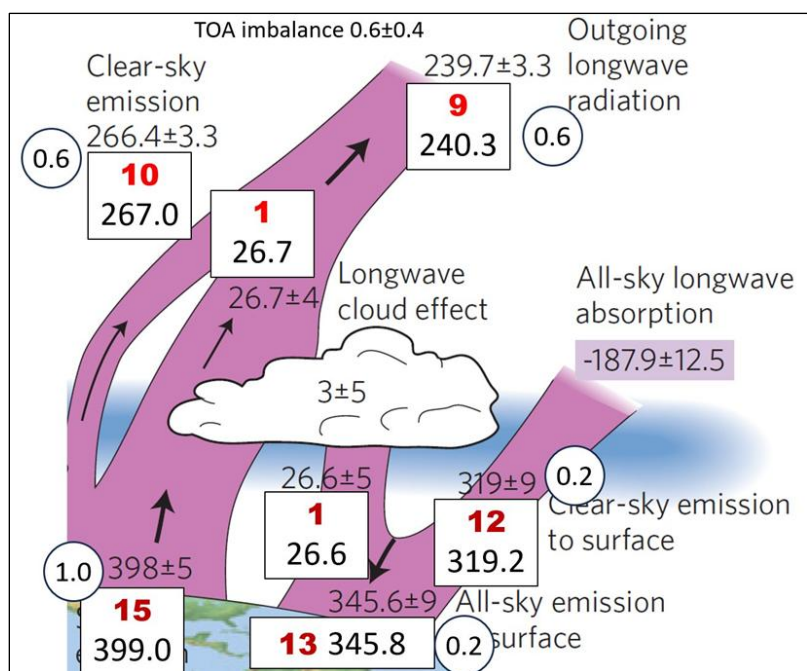
6 At the top of the atmosphere (TOA), integer positions are quarters, that is, they are integers on the  
 7 intercepting cross-section disk to incoming solar radiation, that is, before division by 4 for  
 8 spherical weighting. Incoming solar radiation is smaller than the given lower limit by  $2 \text{ Wm}^{-2}$ .  
 9 Atmospheric window is not part of the system. At the surface, integer position for absorbed solar  
 10 radiation (6 units, with a value of  $159.0 \text{ Wm}^{-2}$ ) falls out the indicated range of 161-168.  
 11 Components of the convective flux (sensible heat and latent heat) do not fit separately into the  
 12 integer system, but their sum (4 units =  $106.0 \text{ Wm}^{-2}$ ) does. The position of total solar irradiance  
 13 (TSI) is 51 units which, using the spherical factor, would be  $1351.5 \text{ Wm}^{-2}$ ; with geodetic weighting  
 14 (factor 4.0034, as in CERES EBAF),  $1352.65 \text{ Wm}^{-2}$ ; still unacceptably low.

15 With these several exceptions, the appearance of the integer ratio system is interesting, but not  
 16 convincing; without further indication, it may be regarded as a simple coincidence.

17 But later in that year, another update on global energy balance was published, based on the then-  
 18 available best global observations (Stephens et al. 2012), where similar structures appear. First,  
 19 the longwave cloud effect at TOA was upgraded to  $26.7 (\pm 4) \text{ Wm}^{-2}$ , resulting in  $\text{TSI} = 51 \text{ units} =$   
 20  $1361.7 \text{ Wm}^{-2}$  (with the spherical multiplying factor of 4), or  $1362.86 \text{ Wm}^{-2}$  (with the geodetic  
 21 formula of 4.0034). Since the then-accepted solar irradiance value was  $\text{TSI} = 1360.8 \pm 0.5 \text{ Wm}^{-2}$   
 22 (Kopp and Lean 2011), the latter would result in  $\text{TSI}/51 = 26.68 \text{ Wm}^{-2}$  in the spherical case, and

1 26.66  $\text{Wm}^{-2}$  in real-Earth geometry, supporting the fine-tuning in LWCRE. Integer positions for  
 2 “Incoming solar” with the CERES geodetic factor of 4.0034 is  $340.14 \text{ Wm}^{-2}$ , and “Reflected solar”  
 3 is  $100.04 \text{ Wm}^{-2}$  ( $340.2$  and  $100.0$  are shown in the diagram).

4 Now with the value of  $26.7 \text{ Wm}^{-2}$ , given as the difference of “Clear-sky emission” ( $266.4$ ) and  
 5 “Outgoing longwave radiation” (all-sky emission,  $239.7$ ) in Fig. B1 of Stephens et al. (2012), these  
 6 values themselves are integer multiples of this unit flux as  $266.4 = 10 \times 26.7$  (and consequently  
 7  $239.7 = 9 \times 26.7$ ) with a difference  $0.6 \text{ Wm}^{-2}$  only, which is far within the stated range of  
 8 uncertainty (3.3), and equivalent to the indicated TOA imbalance. Similarly, at the surface, “Clear-  
 9 sky emission to surface” ( $319$ ) and “All-sky emission to surface” ( $345.6$ ) differ by the longwave  
 10 cloud effect at the surface (LWCRE SFC,  $26.6$ ), and these values are integer multiples of LWCRE  
 11 SFC, as  $319 = 12 \times 26.6$  with a difference of  $0.2 \text{ Wm}^{-2}$ , hence  $345.6 = 13 \times 26.6$  ( $- 0.2 \text{ Wm}^{-2}$ ),  
 12 compared to the stated  $\pm 9 \text{ Wm}^{-2}$  uncertainty. Finally, “Surface emission” ( $398$ ) also occupies an  
 13 integer position, as  $398 = 15 \times 26.6$ , the difference is  $1 \text{ Wm}^{-2}$ , while the indicated uncertainty range  
 14 is  $\pm 5 \text{ Wm}^{-2}$ ; the longwave part is shown in Fig. 2.



15

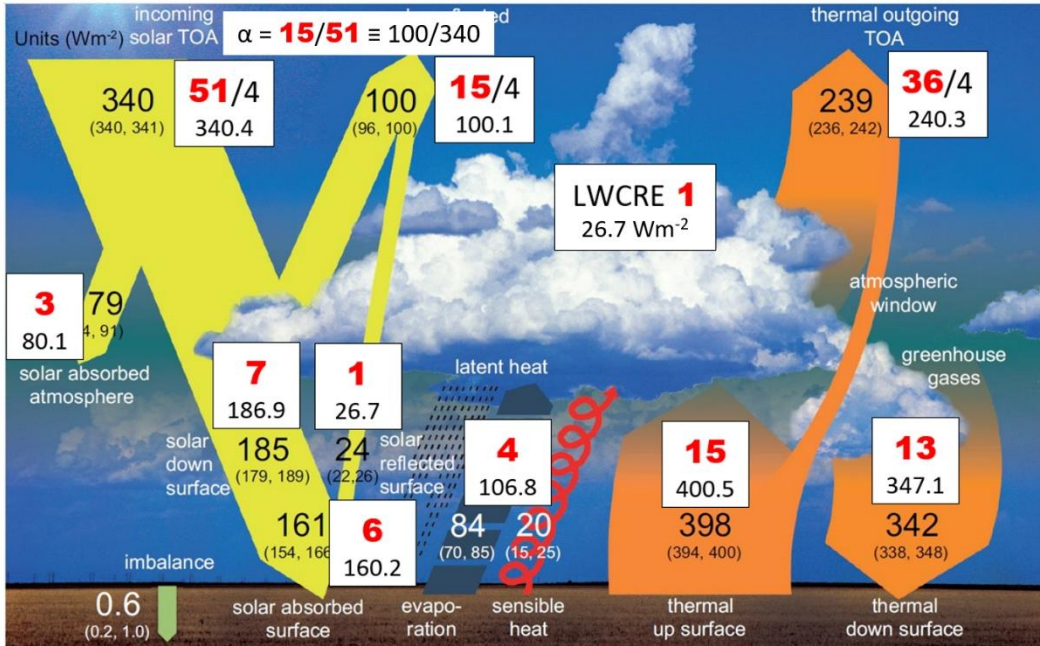
16 **Figure 2** The longwave part of the global annual mean energy budget of Earth (Stephens et al. 2012,  
 17 Fig.B1), with the integer system projected on it in textboxes. Red, bold typeface gives the integer values  
 18 in units of one LWCRE at TOA ( $26.7 \text{ Wm}^{-2}$ ); purple values in units of one LWCRE at the surface ( $26.6$   
 19  $\text{Wm}^{-2}$ ); the differences of the original values and the integer multiples are given in circles in  $\text{Wm}^{-2}$ .

1 Regarding the given uncertainty for LWCRE TOA as  $\pm 4 \text{ Wm}^{-2}$ , from now we will use one  
2 common unit flux for TOA and the surface.

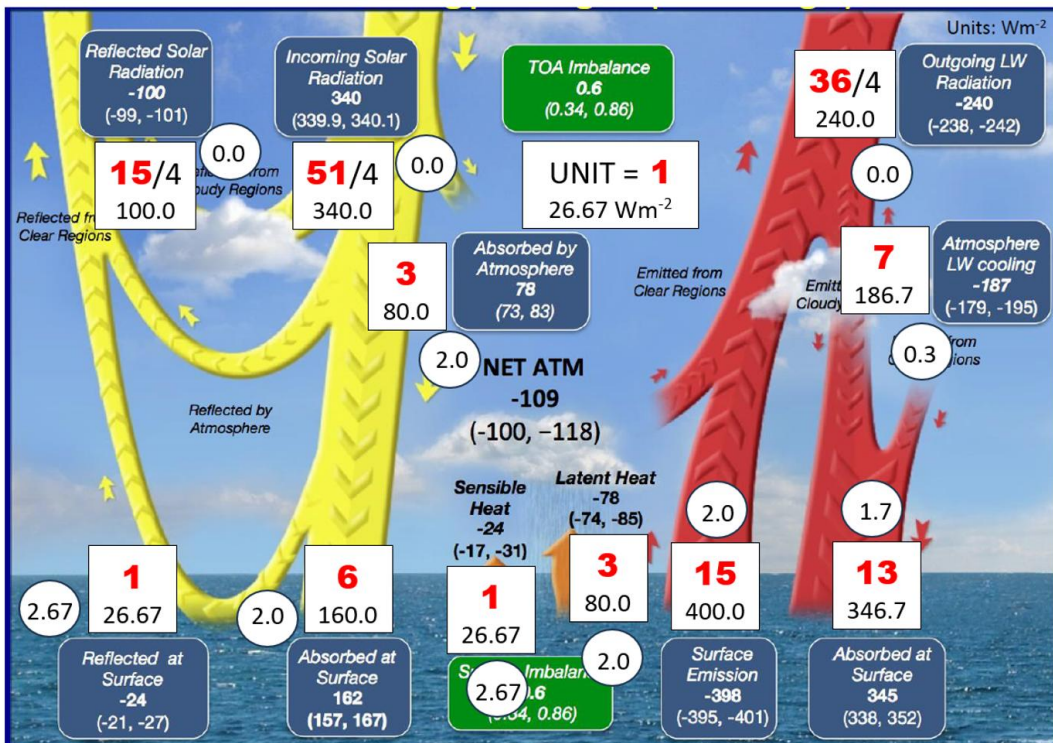
3 Next year, another global mean energy budget distribution was presented (Wild et al. 2013), where  
4 the shortwave components were further updated, resulting in accurate positions in the integer  
5 system when using the same LWCRE TOA of  $26.7 \text{ Wm}^{-2}$  for unit flux as above. At TOA, incoming  
6 solar 340 occupies position of  $51/4 (=340.4)$ , where the division factor of four comes from  
7 spherical weighting; hence total solar irradiance TSI = 51 units =  $1361.7 \text{ Wm}^{-2}$ . Solar reflected  
8 (100) equals  $15/4 = 100.1$  with a difference of  $0.1 \text{ Wm}^{-2}$  only, resulting in an integer ratio for TOA  
9 albedo as  $15/51$ , being arithmetically identical to the indicated  $100/340$ . Absorbed solar and  
10 outgoing thermal radiation in equilibrium are equal with 9 units =  $9 \times 26.7 = 240.3 \text{ Wm}^{-2}$ . Solar  
11 absorbed in the atmosphere is indicated as  $79 \text{ Wm}^{-2}$ ; an integer position is 3 units =  $80.1 \text{ Wm}^{-2}$ ,  
12 allowing solar down to the surface  $185 \text{ Wm}^{-2}$  in the diagram and  $186.9 \text{ Wm}^{-2}$  in the integer system  
13 as 7 units; with  $161 \text{ Wm}^{-2}$  solar absorbed at the surface in the diagram and  $160.2 \text{ Wm}^{-2}$  as 6 units  
14 in the integer system. The largest difference is in “Thermal down surface”, given as  $342 \text{ Wm}^{-2}$ ,  
15 when 13 units =  $347.1 \text{ Wm}^{-2}$ , so the bias is  $5.1 \text{ Wm}^{-2}$ , still within the noted uncertainty; see Fig. 3.

16 Even this discrepancy disappeared next year, when Loeb (2014) published a global mean energy  
17 budget based on CERES EBAF data. Refining the unit flux from  $26.7 \text{ Wm}^{-2}$  to  $26.67 \text{ Wm}^{-2}$ , the  
18 flux component “thermal down surface” (called here “Absorbed at Surface”) in the integer ratio  
19 system is  $346.7 \text{ Wm}^{-2}$ ; with a bias of  $1.7 \text{ Wm}^{-2}$  to the given value of  $345 \text{ Wm}^{-2}$  (this essential flux  
20 component, called also “Back radiation” was regarded as “another measure of the greenhouse  
21 effect” by Inamdar and Ramanathan 1997). The most peculiar feature here is that at the TOA, all  
22 three flux components (Incoming Solar, Reflected Solar and Outgoing LW Radiation) fit to their  
23 integer position with zero difference; see Fig. 4.

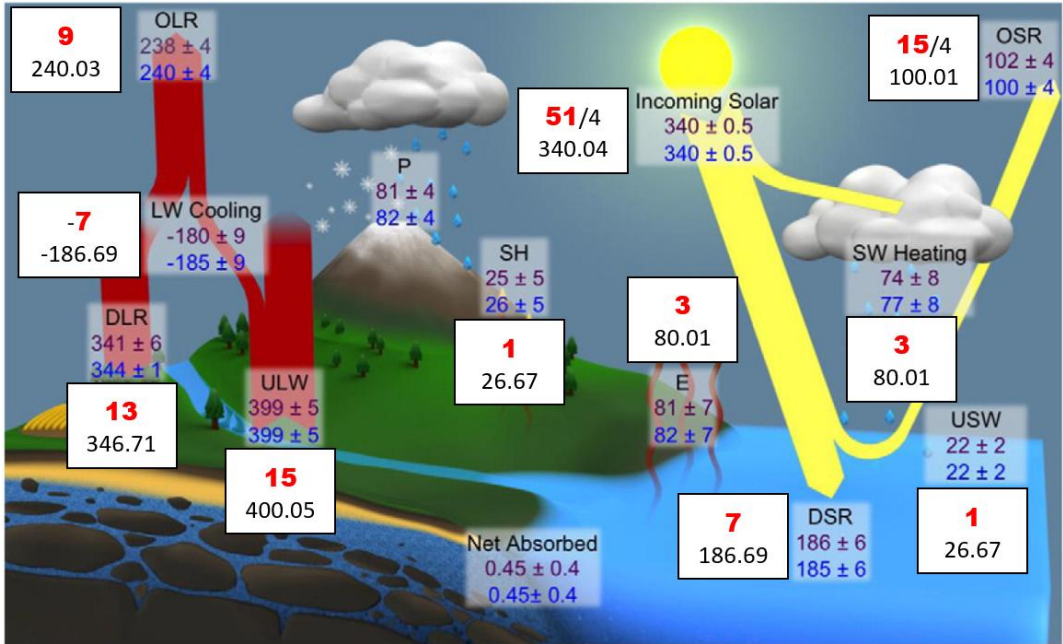
24 Next year again, NASA Energy and Water-cycle Study (NEWS) resulted in a global assessment  
25 of the joint cycles of energy and water (L’Ecuyer et al. 2015, Stephens and L’Ecuyer 2015). The  
26 important improvement here was new, upgraded values proposed to the components of convective  
27 flux separately: sensible heat (SH) =  $25 \text{ Wm}^{-2}$  and  $26 \text{ Wm}^{-2}$ , respectively, and latent heat  
28 (evaporation) =  $81 \text{ Wm}^{-2}$  and  $82 \text{ Wm}^{-2}$ , resp., close to integer positions of 1 unit =  $26.67 \text{ Wm}^{-2}$  and  
29 3 units =  $80.01 \text{ Wm}^{-2}$ . Other flux components in the second-optimized version display well the  
30 integer system, see Fig. 5.



1  
 2 **Figure 3** Integer structure projected a global energy balance from a surface perspective (Wild et al. 2013,  
 3 appeared also in IPCC WGI AR5), using the same unit flux of 26.7 Wm<sup>-2</sup> as above.

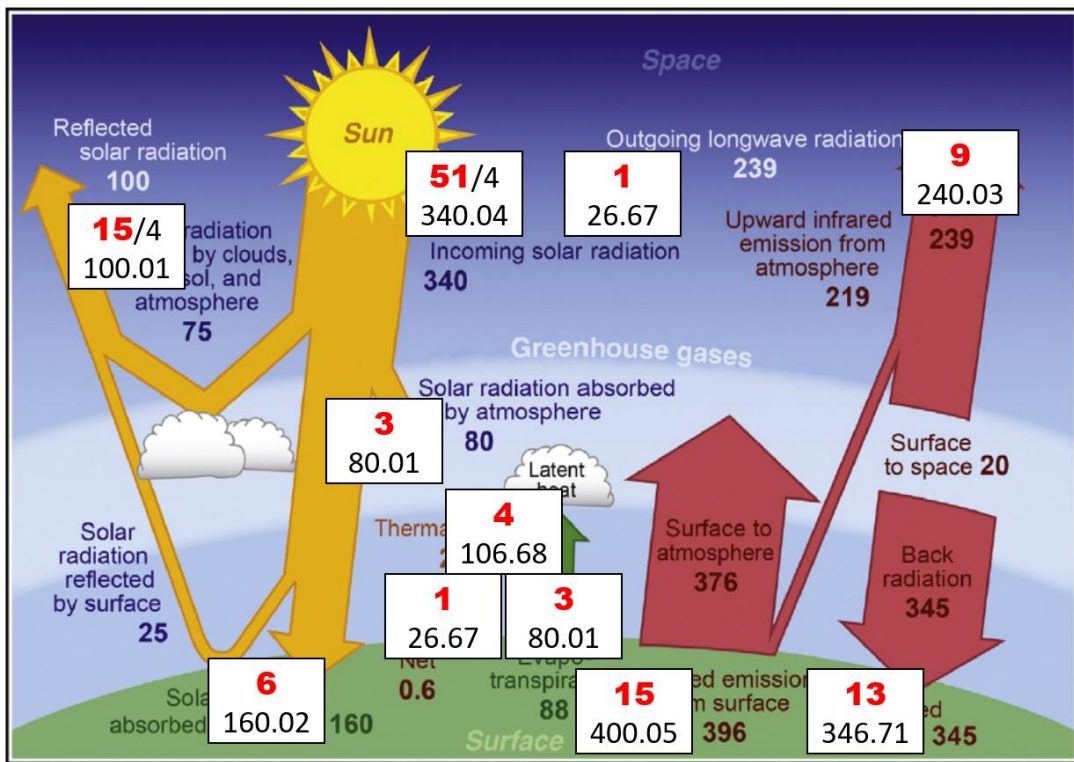


4  
 5 **Figure 4** Integer structure projected a global mean energy budget from CERES EBAF data (Loeb 2014)



1

2 **Figure 5** Global and annual mean Earth's energy balance (Stephens and L'Ecuyer 2015), with integer  
 3 positions projected on it



4

5 **Figure 6** Global and annual average radiative and non-radiative energy-flow diagram for Earth and its  
 6 atmosphere (Hartmann 2016, Fig. 2.4), with the integer system projected on it.

1 The increased value of  $345 \text{ Wm}^{-2}$  was accepted for the “Back radiation” in the second edition of  
 2 Hartmann (2016). Using the same unit flux of  $26.67 \text{ Wm}^{-2}$  as above, the solar components of the  
 3 energy flow system fit into the integer system within a robust accuracy of  $0.04 \text{ Wm}^{-2}$ ; the largest  
 4 difference is in the infrared emission from the surface, which was decreased from the IPCC and  
 5 CERES EBAF value by  $2 \text{ Wm}^{-2}$ , to  $396 \text{ Wm}^{-2}$ . The components of the convective flux do not  
 6 occupy integer positions separately; see Figure 6.

7 In the past decade, this higher value for the downward longwave radiation became widely  
 8 accepted. In a current assessment of the global radiation budget from a surface perspective (Li, Li,  
 9 Wild and Jones, 2024) based on 34 CMIP6 models, SW down radiation to the surface is  $186 \pm 6$ ,  
 10 Reflect by surface =  $24 \pm 3$ , convective flux (sensible heat + latent heat) = 106, Thermal down  
 11 surface =  $346 \pm 6$ , and Thermal up surface =  $402 \pm 5 \text{ [Wm}^{-2}]$ . The corresponding integer positions,  
 12 with the same unit flux of  $26.67 \text{ Wm}^{-2}$  are as follows: 7 units = 186.69, 1 unit = 26.67, 4 units =  
 13 106.68, 13 units = 346.71, and 15 units = 400.05  $[\text{Wm}^{-2}]$ ; the differences are 0.69; 2.67; 0.68; 0.71,  
 14 and 1.95  $[\text{Wm}^{-2}]$ , respectively — each of them far within the indicated uncertainty range.

15 At the top of the atmosphere, Stackhouse et al. (2024) provide a radiation budget from CERES  
 16 satellite observations for 2001-2022. As shown in Table 1, with an upgraded unit flux of  $26.68$   
 17  $\text{Wm}^{-2}$ , the difference of their climatological mean from the integer positions falls within, or close  
 18 to (in the case of ASR), the interannual variability for the same period. Data taken from their Table  
 19 2.9.

20 **Table 1** Global mean TOA radiative fluxes (Climatological Mean and Interannual Variability) from  
 21 CERES, compared to the integer positions

Global	N	$N \times \text{unit}$ unit = $26.68$ $\text{Wm}^{-2}$	Climatological Mean 2001-22 $\text{Wm}^{-2}$	Difference $\text{Wm}^{-2}$	Interannual Variability 2001-22, $\text{Wm}^{-2}$
OLR	36/4	240.12	240.35	0.23	$\pm 0.65$
TSI	51/4	340.17	340.20	0.03	$\pm 0.15$
RSW	15/4	100.05	99.00	1.05	$\pm 1.05$
ASR	36/4	240.12	241.20	1.08	$\pm 1.05$
Net	0	0	0.85	0.85	$\pm 0.85$

22

1 The accuracy altogether is much better than expected from a simple coincidence, therefore an  
2 intense quest for a possible physical science basis was initiated. Four radiative transfer equations  
3 were identified and verified on published global energy flow distributions of CERES and GEWEX  
4 data, from which the integer ratios for the principal components arise as a solution.

## 5 **Results**

6 We utilize Schwarzschild's (1906, Eq. 11) two-stream radiative equilibrium model, consisting of  
7 three relationships (reproduced here in facsimile from the original;  $E$  emission of the surface;  $A$   
8 upward beam,  $B$  downward beam given as the function of  $A_0$ , the emerging flux at the top-of-  
9 atmosphere, and  $m$ , the „optische Masse“, optical depth):

$$(11) \quad E = \frac{A_0}{2}(1 + m), \quad A = \frac{A_0}{2}(2 + m), \quad B = \frac{A_0}{2}m.$$

10

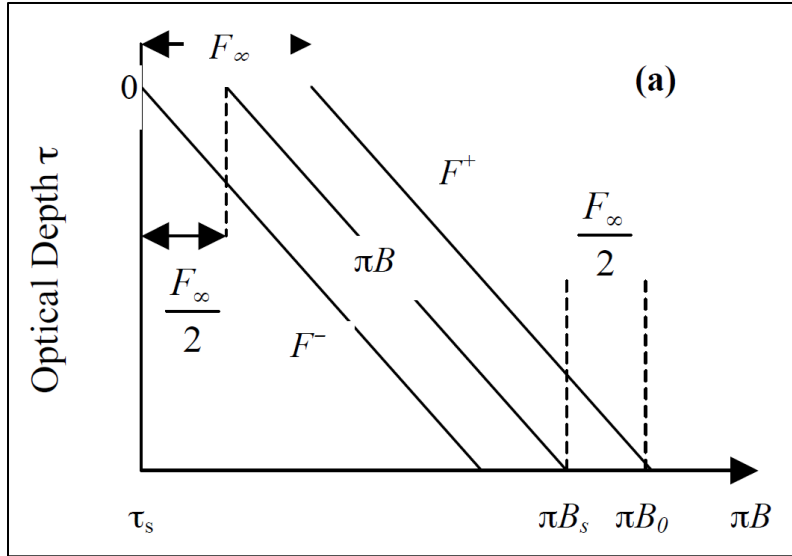
11 Our first equation will be the difference of the second and first terms:

12

$$\text{Eq. (1)} \quad A - E = \Delta A = A_0/2,$$

13 yielding the net radiation at the surface, independently of the optical depth. It is reproduced and  
14 graphically represented in standard university textbooks like Goody (1964, Eq. 2.115); Houghton  
15 (1977, 1986, 2002, Eq. 2.13, Fig. 2.4); Chamberlain (1978, 1987, Eq. 1.2.29, Fig.1.4); Goody and  
16 Yung (1989, Eq.2.146); Hartmann (1994, 2016, Eqs. 3.48-3.54); Salby (1996, 2012, Eq. 8.67, Fig.  
17 8.20); Pierrehumbert (2008, Eq. 4.45); Ambaum (2021, Eq. 10.56), and in university lecture notes  
18 (Stephens 2003, Eqs. 6.10a-b, Fig. 6.3a:  $\pi T_S^4 - \pi T(\tau_S)^4 = \pi B_S - \pi B_0 = F_{\infty}/2$ ), see Fig.7.





1

2 **Figure 7** The flux profiles and blackbody function predicted by the simple gray body model as a function  
 3 of optical depth (Stephens 2003, Fig. 6.3a)

4 Emden (1913) realized soon that in radiative equilibrium, Eq. (1) represents a temperature  
 5 discontinuity at the surface, but in the same sentence he added that this jump (*Temperatursprung*)  
 6 “is greatly diminished by conduction of heat and evaporation”. Authors generally note that “such  
 7 a steep lapse rate is very unstable with respect to vertical motion, and will soon be destroyed by  
 8 the process of convection” (Houghton 1977); “such discontinuities are usually are greatly  
 9 suppressed in reality because of efficient heat transport by conduction and convection” (Hartmann  
 10 1994); “The solutions in Eqns. (6.10a) and (6.10b) predict a discontinuity between the surface  
 11 temperature  $T_s$  and the air temperature just above the ground  $T(\tau_s)$ ”, and adds: “This radiative  
 12 equilibrium profile is unstable w.r.t. vertical motion and is destroyed by convection” (Stephens  
 13 2003); “This temperature discontinuity is unstable in practice and there will be turbulent heat  
 14 exchange which will remove the temperature discontinuity” (Ambaum 2021).

15 The equation states that the net radiation at the surface ( $R_N$ ) in radiative equilibrium — and the  
 16 corresponding convection in radiative-convective equilibrium — equals half of the outgoing  
 17 longwave radiation (OLR) in the clear-sky:

18 Eq. (1)  $R_N$  (clear-sky) = SFC (SW net + LW net) (clear-sky) =  
 19 (SW down – SW up) + (LW down – LW up) (clear-sky) = OLR (clear-sky)/2.

1 As an initial justification, the equation was controlled on the then-available NASA CERES dataset,  
2 Energy Balanced and Filled (EBAF-Surface) Edition 2.8, data were taken from the Data Quality  
3 Summary (2015), Table 4.1:

4 Eq. (1)  $R_N$  (clear-sky) = SW down – SW up + LW down – LW up (clear-sky) = OLR(clear-sky)/2.

5 
$$243.9 - 29.7 + 316.0 - 398.0 = 265.7/2 - 0.65$$

6 The equation is valid on that data product with a difference of  $0.65 \text{ Wm}^{-2}$ . [Note that Earth's heat  
7 uptake in that time was estimated as  $0.58 \pm 0.38 \text{ Wm}^{-2}$  (Loeb et al. 2012).]

8 Since the first equation prescribes the convective flux (the sum of the sensible heat flux and latent  
9 heat flux) in a direct relationship to the outgoing longwave radiation (OLR) at TOA in the clear-  
10 sky, and convection changes almost linearly with sea surface temperature, a definite OLR-  
11 dependent convection assumes a definite, OLR-dependent surface upward longwave (ULW)  
12 thermal emission. Exploring possible formulas, as the optical depth ( $\tau$ ) of zero defines TOA, and  
13  $\tau = 1$  the level where OLR is initiated, Schwarzschild's formula for the surface (the middle term  
14 in Eq. 11) was tried at  $\tau = 2$ . Then the second equation gives the total SW + LW absorbed radiation  
15 ( $R_T$ ) at the surface in the clear-sky:

16 Eq. (2)  $R_T$  (clear-sky) = (SW down – SW up + LW down) (clear-sky) = 2OLR(clear-sky).

17 CERES EBAF-Surface Ed2.8 Data Quality Summary (DQS) data [17]:

18 
$$243.9 - 29.7 + 316.0 = 2 \times 265.7 - 1.2 \text{ Wm}^{-2}.$$

19 This accuracy (compared to the estimated uncertainties in the EBAF-Surface data of  $1\sigma$  between  
20 3 and  $7 \text{ Wm}^{-2}$ , see Table 4.2 of [17]) was convincing enough to proceed further in this direction.

21 For all-sky, a third and fourth equations were created from the first pair, by separating atmospheric  
22 radiation transfer from the longwave effect of clouds (LWCRE) and using all-sky data on both  
23 sides:

24 Eq. (3)  $R_N$  (all-sky) = Surface SW net + LW net (all-sky) = [OLR(all-sky) – LWCRE]/2;

25 and

1 Eq. (4)  $R_T$  (all-sky) = Surface (SW + LW) absorbed (all-sky) = (SW down – SW up + LW down)  
 2 (all-sky) = 2OLR (all-sky) + LWCRE.

3 Their accuracy on that data product was  $2.65 \text{ Wm}^{-2}$  for Eq. (3) and  $2.10 \text{ Wm}^{-2}$  for Eq. (4).

4 Controlling the four equations on EBAF Ed4.1\_V3 data product, we have the biases of the  
 5 individual equations within the range of  $\pm 2.83 \text{ Wm}^{-2}$ ; and the mean bias of the four equations is  
 6  $0.0007 \text{ Wm}^{-2}$  (this justifies the use of four decimal places in the netCDF file), see Table 2. EBAF  
 7 Edition 4.2 is also checked; with Version 4 data, first on the same period (April 2000-March 2022);  
 8 the differences become as follows: -2.35, -2.70, 3.98, 3.46; the mean bias is  $0.60 [\text{Wm}^{-2}]$ ; then on  
 9 the extended time period April2000-March 2024, and have -2.32, -2.50, 4.01, 3.67, with a mean  
 10 of  $0.715 [\text{Wm}^{-2}]$ , still far within the absolute calibration uncertainty of the CERES instrument, and  
 11 in the magnitude of the estimated Earth’s Energy Imbalance.

12 **Table 2** Verification of the four equations on CERES EBAF data

13 CERES EBAF Edition 4.1 Version 3, 22 years (April 2000 – March 2022) ( $\text{Wm}^{-2}$ )  
 14 CERES EBAF Edition 4.2 Version 4, 22 years (April 2000 – March 2022) ( $\text{Wm}^{-2}$ )  
 15 CERES EBAF Edition 4.2 Version 4, 24 years (April 2000 – March 2024) ( $\text{Wm}^{-2}$ )

Eq. (1) $R_N$ clear	SFC SW dn	–SW up	+ LW down	–LW up	TOA LW/2	Diff
Ed4.1, 22-yr	240.8680	–29.0724	+317.4049	–398.5211	266.0122 /2	–2.3267
Ed4.2, 22-yr	241.0969	–29.7521	+317.8744	–398.5890	265.9594 /2	–2.3495
Ed4.2, 24-yr	241.0514	–29.7043	+318.0984	–398.7742	265.9748 /2	–2.3161
Eq. (2) $R_T$ clear	SFC SW dn	– SW up	+ LW down		$2 \times \text{TOA LW}$	Diff
Ed4.1, 22-yr	240.8680	–29.0724	+ 317.4049		$2 \times 266.0122$	–2.8238
Ed4.2, 22-yr	241.0969	–29.7521	+ 317.8744		$2 \times 265.9594$	–2.6996
Ed4.2, 24-yr	241.0514	–29.7043	+ 318.0984		$2 \times 265.9748$	–2.5042
Eq. (3) $R_N$ all	SFC SW dn	– SW up	+ LW down	– LW up	$(\text{TOA LW} - \text{LWCRE})/2$	Diff
Ed4.1, 22-yr	186.8544	–23.1629	+345.0108	–398.7550		+2.7083
Ed4.2, 22-yr	187.1451	–23.4950	+346.1057	–398.4220		+3.9818
Ed4.2, 24-yr	187.1756	–23.4607	+346.3158	–398.6162		+4.0126
Eq. (4) $R_T$ all	SFC SW dn	– SW up	+ LW down		$2 \times \text{TOA LW} + \text{LWCRE}$	Diff
Ed4.1, 22-yr	186.8544	– 23.1629	+ 345.0108		$2 \times 240.2450 + 25.7672$	+2.4450
Ed4.2, 22-yr	187.1451	– 23.4950	+ 346.1057		$2 \times 240.3317 + 25.6277$	+3.4647
Ed4.2, 24-yr	187.1756	– 23.4607	+ 346.3158		$2 \times 240.3894 + 25.5854$	+3.6665
Mean						0.0007
						0.5994
						0.7147

1 This unprecedented accuracy of the constraint equations raises a couple of questions. Do these  
 2 four equations express an arithmetic identity? The answer is no; in the prevailing theory we are  
 3 not aware of any relationship that would require these couplings between surface and TOA  
 4 irradiances, without referring to any atmospheric gaseous composition or the optical depth. Or, are  
 5 these four equations built in the CERES data production protocol? No again: the mean bias in the  
 6 first five years vary between -0.5 and -0.2 [ $\text{Wm}^{-2}$ ] and it approaches zero after including 17 years  
 7 into the averaging; then it occupies the value of zero and remains there after only two decades.

8 Notice that the clear-sky equations prescribe the ratio

$$9 \quad R_N : (\text{TOA\_LW\_up}) : (\text{SFC\_LW\_up}) : R_T = 1 : 2 : 3 : 4 ,$$

10 resulting in a clear-sky greenhouse factor of

$$11 \quad g(\text{clear-sky}) = G(\text{clear-sky}) / (\text{SFC\_LW\_up}) = [(\text{SFC\_LW\_up}) - (\text{TOA\_LW\_up})] / (\text{SFC\_LW\_up})$$

$$12 \quad = 1/3.$$

13 With CERES EBAF Edition 4.2 V4 (24-yr) data (Table 1),  $g(\text{clear-sky, CERES}) = (398.7742 -$   
 14  $265.9748) / 398.7742 = 0.3330.$

15 Recently, data were published from global energy and water cycle assessments on 30 years of the  
 16 GEWEX mission (Stephens et al. 2023). Their data are for all-sky, therefore only equations (3)  
 17 and (4) maybe controlled, with LWCRE taken from an earlier study of the same authors (Stephens  
 18 et al. 2012) as  $26.7 \text{ Wm}^{-2}$ . According to Fig. 2 of the GEWEX study, net radiation at the surface  
 19 ( $R$ ) equals the sum of the convective fluxes: latent heat (evaporation) and sensible heat. Using data  
 20 from Fig. SB3,

$$21 \quad \text{Eq. (3)} \quad R_N = LE + H = \text{"Evaporation"} + \text{"Sensible heat"} = (\text{"Outgoing LW"} - \text{LWCRE})/2$$

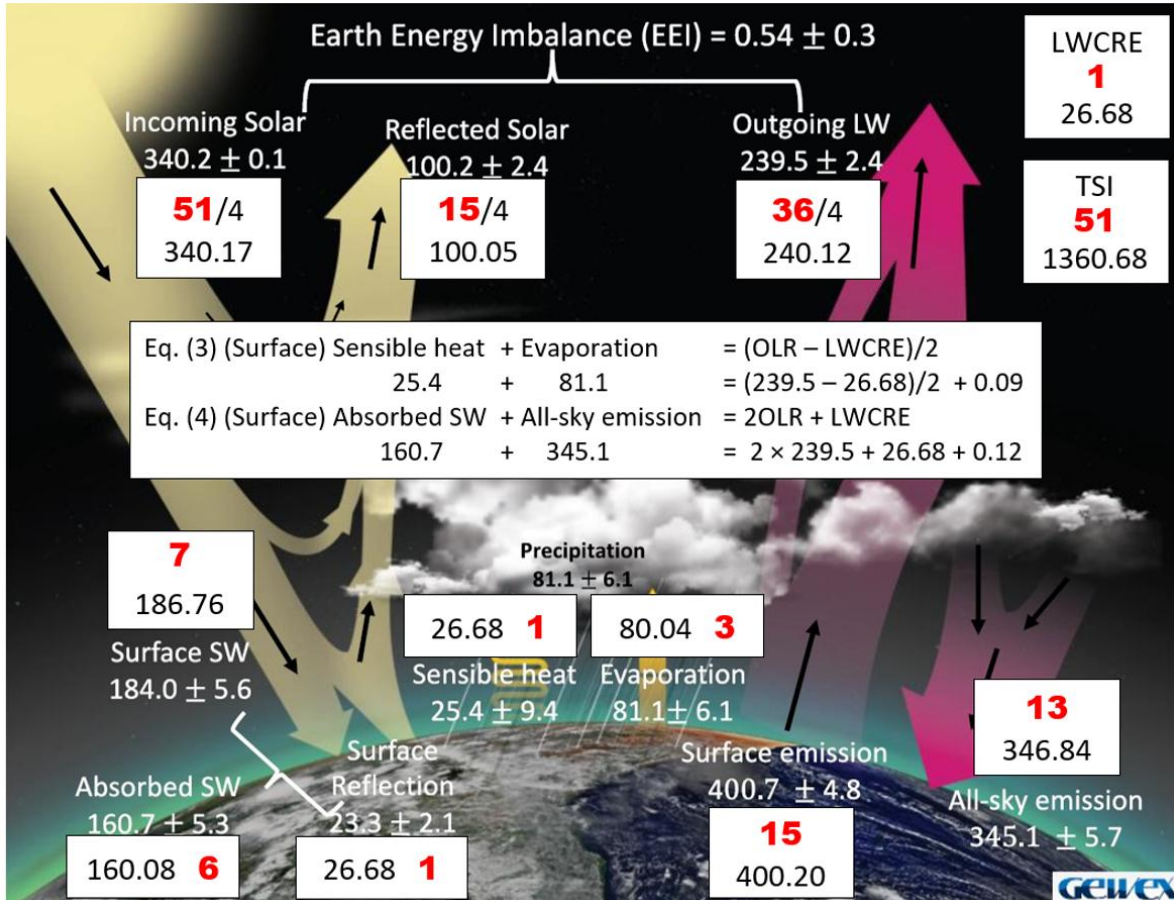
$$22 \quad 81.1 + 25.4 = (239.5 - 26.7)/2 + 0.1 [\text{Wm}^{-2}]$$

$$23 \quad \text{Eq. (4)} \quad R_T = \text{"Surface SW"} - \text{"Surface Reflection"} + \text{"All-sky emission"} = 2 \times \text{"Outgoing LW"} +$$

$$24 \quad \text{LWCRE}$$

$$25 \quad 184.0 - 23.3 + 345.1 = 2 \times 239.5 + 26.7 + 0.1 [\text{Wm}^{-2}]$$

26 On GEWEX data, both the all-sky equations are valid within  $0.1 \text{ Wm}^{-2}$ ; see Fig. 8.



1

2 **Figure 8** The all-sky (third and fourth) equations and the integer structure is projected on the GEWEX  
 3 dataset, based on 30 years of data collection (Stephens et al. 2023). The unit flux of LWCRE is a refined  
 4 value from  $26.7 \text{ Wm}^{-2}$  from Stephens et al. (2012) to  $26.68 \text{ Wm}^{-2}$  as the most accurate fit to TSI.

5 As a comparison, Eq. (3) for convection with the data of Stevens and Schwartz (2012, Table 1),  
 6 with  $LWCRE = 26.67 \text{ Wm}^{-2}$ : Sensible heat + Latent heat (106) =  $(OLR - LWCRE)/2$  [ $(239 -$   
 7  $26.67)/2 = 106.165$ ], the difference is  $0.165 \text{ Wm}^{-2}$ , and Eq. (4) Solar absorbed surface (162) +  
 8 Back radiation (342) =  $2OLR + LWCRE$  (504.67), the difference is  $0.67 \text{ Wm}^{-2}$ .

9 The same with Hartmann's (2016, Fig.2.4) data: Eq. (3) Sensible heat + Latent heat (108) =  $(OLR$   
 10  $- LWCRE)/2$  (106.17) is valid with a difference of  $1.83 \text{ Wm}^{-2}$ , and Eq. (4), Solar absorbed surface  
 11 (160) Back radiation (345) =  $2OLR + LWCRE$  (504.67) with a difference of  $0.33 \text{ Wm}^{-2}$ .

12

13

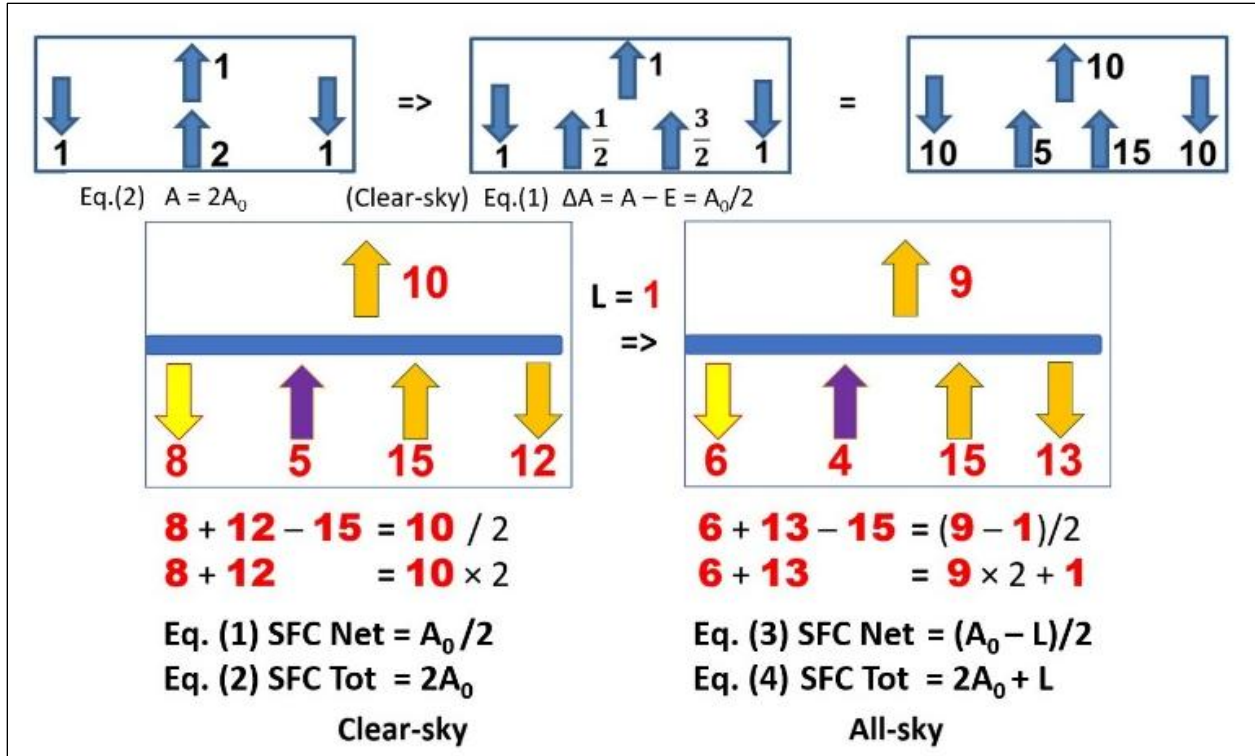
## 1 Discussion

### 2 The integer solution

3 As the equations are not direct functions of  $\tau$ , a stationary (geometric) representation may be  
4 applied (Fig.9). Let's start with the second equation, stating the equality of the total energy  
5 absorbed (and emitted) by the surface to twice the OLR under clear-sky. This case is described by  
6 the simplest greenhouse model, see for example Hartmann (1994, Fig. 2.3), representing the flux  
7 ratios of  $A = 2A_0$  [in Schwarzschild's (1906, Eq. 11) notation] as shown in the upper left panel;  
8 Equation (1) is represented in the upper middle panel as  $\Delta A = A - E = A_0/2$  and  $E = (3/2)A_0$  (for  
9 its simple derivation, see Hartmann 1994, Fig. 3.11 and Eq. 3.54).

10 These three relationships [Eq. (1) as  $\Delta A = A - E = A_0/2$ , Eq. (2) as  $A = 2A_0$ , and their immediate  
11 corollary,  $E = (3/2)A_0$ ] can be identified on a recently published geometric greenhouse model  
12 (Trenberth 2022); for details and its application on the real-Earth atmosphere, see video in the  
13 Supplementary Material.

14 In the right panel of the upper row, the ratios are the same as in the middle, multiplied by 10 (since  
15 the unit is not specified yet). Then, introducing the red unit (for LWCRE), and keeping in mind  
16 that if Upward LW at TOA is 10 units (of LWCRE) in the clear-sky, then it must be 9 units in the  
17 all-sky; and if Downward LW is 12 units in the clear-sky, then it will be 13 units in the all-sky,  
18 with the constraint that Upward LW at the surface is the same in both cases, we have an integer  
19 ratio system, as shown in Fig.9.



1

2 **Figure 9** Stationary (geometric) representation of the four equations, with integer solution as multiples of  
 3 the unit flux of  $L$  (representing LWCRE).

4 Validity of equations and the extended set of the integers on CERES data are given in Table 3.  
 5 The fit of components not included in the equations (for example, TOA SW up both in clear-sky  
 6 and all-sky) is remarkable. Notice that the components of convective flux in the GEWEX study  
 7 (based on the NEWS – NASA Energy and Water-cycle Study methodology, L’Ecuyer et al. 2015)  
 8 occupy integer positions separately.

9

10 **Table 3** The four equations and the integer positions for the clear-sky and all-sky global mean energy  
 11 flow system, including TSI, using the unit flux of  $26.68 \text{ Wm}^{-2}$  as the best fit on CERES EBAF Ed4.2 data,  
 12 and the differences. The greenhouse effect is also shown.

**Data: CERES EBAF Ed4.2 Version 2, October 2000 – September 2023**

Eq. (1)  $8 + 12 - 15 = 10/2$ ; Eq. (2)  $8 + 12 = 10 \times 2$ ;

Eq. (3)  $6 + 13 - 15 = (9 - 1)/2$ ; Eq. (4)  $6 + 13 = 9 \times 2 + 1$        $1 = 26.68 \text{ Wm}^{-2}$

<b>TSI = 51</b> Clear-sky	<b>N</b>	<b>N</b> × Unit ( $\text{Wm}^{-2}$ )	EBAF Ed4.2 ( $\text{Wm}^{-2}$ )	Diff ( $\text{Wm}^{-2}$ )
TOA LW up	<b>40/4</b>	266.80	265.95	-0.85
TOA SW up	<b>8/4</b>	53.36	53.78	0.42
TOA SW net	<b>3/4</b>	20.01	20.47	0.46
SFC SW net	<b>8</b>	213.44	211.33	-2.11
SFC LW down	<b>12</b>	320.16	318.06	-2.10
SFC LW up	<b>15</b>	400.20	398.58	-1.62
G	<b>5</b>	133.40	132.63	-0.77
<b>TSI = 51</b> All-sky				
TOA LW up	<b>36/4</b>	240.12	240.37	0.25
TOA SW up	<b>15/4</b>	100.05	98.95	-1.10
SFC SW net	<b>6</b>	160.08	163.71	3.63
SFC LW down	<b>13</b>	346.84	346.25	-0.59
SFC LW up	<b>15</b>	400.20	398.75	-1.45
G	<b>6</b>	160.08	158.38	-1.70

1

2

3 **Summary**

4 We recognized small integer ratios between the components of the global mean energy flow  
 5 system; the fundamental ratios are identified as the solution of four radiative transfer equation  
 6 having their origin in Schwarzschild's (1906) plane-parallel approximation. Both the ratios and  
 7 the equations are consistent to global observations of CERES and GEWEX within uncertainty.

8 As an independent estimate, we recall here the clear-sky greenhouse effect from the GFDL  
 9 Atmospheric Model 4 (Raghuraman et al. 2019), where its value is referred as  $133.4 \pm 0.6 \text{ Wm}^{-2}$ .  
 10 Notice that the clear-sky greenhouse factor is  $g(\text{clear-sky}) = G / \text{SFC LW up} = 5/15 = 1/3$  in the  
 11 integer system and  $132.63/398.58 = 0.333$  with CERES data. The integer position for the all-sky  
 12 greenhouse factor is  $g(\text{all-sky}) = 6/15 = 0.4$ , while CERES data gives  $158.38/398.75 = 0.397$ .

13 Using IPCC AR6 data (Forster et al. 2021, Fig. 7.2), the three fundamental climate parameters  
 14 (Bengtsson 2012) are: Total solar irradiance (51 units in the integer system,  $1360.68 \text{ Wm}^{-2}$ );  
 15 planetary albedo (15/51, arithmetically identical to 100/340), and planetary emissivity (TOA LW  
 16 up / SFC LW up;  $9/15 = 0.6$  as integer ratio, compared to  $239/398 = 0.6005$ ).



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